

- Rigid Body Motion - preserves distance between points
 - $\|p(t) - q(t)\| = \|p(0) - q(0)\|$ distance is constant
 - $g: O \rightarrow \mathbb{R}^3$ - mapping; $g(p) = g(p) - g(o)$
 - $g = (v \times \omega) + g_a(v) + g_a(\omega)$ compute it
 - we use right-handed frames, $z = x \times y$

- Rotational Motion
 - R_{AB} - axes of B written in terms of A
 - = [x_B y_B z_B] column vectors
 - orthogonal $R, R^T = R^{-1} = I$
 - $\det(R) = 1$ // right handed
 - $SO(n) = \{R \in \mathbb{R}^{n \times n} : RR^T = I, \det R = +1\}$
 - group - closure, identity, inverse, associativity
 - R_{AB} also rotates point from frame B to frame A
 - $q_a = R_{AB} q_b$
 - $R_{AC} = R_{AB} R_{BC}$
 - $\hat{a} = (a)^{\wedge} = \begin{bmatrix} 0 & -a_2 & a_3 \\ a_2 & 0 & -a_1 \\ -a_3 & a_1 & 0 \end{bmatrix}$ cross product $a \times b = (a)^{\wedge} b$, $\hat{a}^T = -\hat{a}$
 - $R(\omega)^{\wedge} R^T = (R\omega)^{\wedge}$ unit
 - $R(\omega, \theta) = e^{\hat{\omega}\theta}$ // rotate about $\hat{\omega}$ by θ
 - $so(n) = \{S \in \mathbb{R}^{n \times n} : S^T = -S\}$
 - $\hat{a}^2 = -aa^T - \|a\|^2 I$
 - $\hat{a}^3 = -\|a\|^2 \hat{a}$

- Rodrigues' formula
 - $e^{\hat{\omega}\theta} = I + \frac{\hat{\omega}\theta}{\|\omega\|} \sin(\|\omega\|\theta) + \frac{\hat{\omega}^2 \theta^2}{2\|\omega\|^2} (1 - \cos(\|\omega\|\theta))$
- Euler Angles - (α, β, γ) - rotate about multiple axis
 - $R_{\alpha\beta\gamma} = R_z(\gamma) R_y(\beta) R_x(\alpha)$ also find in the matrix form
- 2x Euler (yaw, pitch, roll) - fixed axis (fixed point)
- 3 dimensional rep of rotation always has 3 independent (yaw, pitch, roll)
- Quaternion - $q = [1, q_1, q_2, q_3]^T$
 - $\theta = 2 \cos^{-1}(q_0)$, $\omega = [\frac{2q_1}{\sin(2\theta)}, \frac{2q_2}{\sin(2\theta)}, \frac{2q_3}{\sin(2\theta)}]^T$ if $\theta \neq 0$

- Rigid Motion
 - translation and rotation
 - p is origin of B in A
 - $SE(3) = \{g(p, R) = p e^{R\theta}, R \in SO(3)\} \cong \mathbb{R}^3 \times SO(3)$
 - $q_a = p_a + R_{ab} q_b = g_a(q_b)$
 - $g_a(v) = R_{ab} v_b$ vectors
 - Homogeneous Representation
 - point $\begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix}$ with $\begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix}$
 - $\bar{q}_a = \begin{bmatrix} q_a \\ 1 \end{bmatrix} = \begin{bmatrix} R_{ab} & p_a \\ 0 & 1 \end{bmatrix} \begin{bmatrix} q_b \\ 1 \end{bmatrix} = \bar{g}_{ab} \bar{q}_b$
 - $\bar{g}_{ab} = \bar{g}_{ab} \bar{g}_{bc}$
 - $\bar{g}^{-1} = \begin{bmatrix} R^T & -R^T p \\ 0 & 1 \end{bmatrix}$
 - $\hat{\xi} = \begin{bmatrix} \hat{\omega} & v \\ 0 & 0 \end{bmatrix}$ // rotate about ω and pt. v twist
 - $v = -\omega \times p$
 - $so(3) = \{(\omega, v) : \omega \in \mathbb{R}^3, v \in \mathbb{R}^3\}$
 - $\begin{bmatrix} \hat{\omega} & v \\ 0 & 0 \end{bmatrix}^T = \begin{bmatrix} \hat{\omega} & 0 \\ 0 & 0 \end{bmatrix}$
 - $\begin{bmatrix} \hat{\omega} & v \\ 0 & 0 \end{bmatrix}^{\wedge} = \begin{bmatrix} \hat{\omega} & 0 \\ 0 & 0 \end{bmatrix}$
 - $e^{\hat{\xi}\theta} \in SE(3)$ pushed by ω
 - all $SE(3)$ has $\alpha(\xi)$ pushed by ω

- Screw
 - rotate about axis, then translate
 - h : angle, h is pitch
 - h : pitch - distance between
 - l : line $\{q + \lambda w : \lambda \in \mathbb{R}\}$
 - screw to twist, use unit twist
 - $h = \omega \theta$, $\|h\| = l$ // unit = 1 or $\omega = \omega \theta$, $\|h\| = l$
 - $\hat{\xi} = \begin{bmatrix} \hat{\omega} & v \\ 0 & 0 \end{bmatrix}$
 - $h = \omega \theta$, $\|h\| = l$
 - $\hat{\xi} = \begin{bmatrix} \hat{\omega} & -\omega \times q + hw \\ 0 & 0 \end{bmatrix}$
 - $e^{\hat{\xi}\theta} = \begin{bmatrix} e^{\hat{\omega}\theta} & (I - e^{\hat{\omega}\theta})(\omega \times v) + \omega \omega^T v \theta \\ 0 & 1 \end{bmatrix}$
 - $g e^{\hat{\xi}\theta} g^{-1} = e^{(Ad_g \hat{\xi})\theta}$ $Ad_g \xi$ is new axis of ξ after transform by g

- Kinematics
 - Forward Kinematics
 - joint space Q - all possible configs
 - S^1 - angles for revolute
 - \mathbb{R} - for prismatic
 - base frame S
 - tool frame T
 - Product of Exponentials
 - get limit at $\theta = 0$
 - order doesn't matter? depends: Mark
 - $g_{S^1}(\theta) = e^{\hat{e}_i \theta_1} \dots e^{\hat{e}_n \theta_n}$
 - choice of base frame can simplify things
 - David-Holten's Parameterization
 - 4 joints & 4 axes: $\alpha_i, a_i, d_i, \theta_i$
 - prismatic $\theta_i = d_i$: revolute
 - revolute $\theta_i = \alpha_i$: prismatic
 - pile of cancellations occur
 - twist are relative to previous link
 - Manipulator Workspace
 - reachable workspace $W_R = \{p(\theta) : \theta \in Q\} \subset \mathbb{R}^3$
 - dexterous workspace $W_D = \{p \in \mathbb{R}^3 : \forall R \in SO(3), \exists \theta \text{ s.t. } g(\theta) = (p, R)\} \subset \mathbb{R}^3$
 - not easy to calculate
 - has spherical workspace (3 links) so $W_D = W_R$

- Inverse Kinematics
 - desired config $g_d = g(\theta)$, $\theta?$
 - Paden-Kahane subproblems
 - Subproblem 1 - Rotate about 1 axis
 - $e^{\hat{e}_1 \theta} p = q$
 - 0, 1, 2, or infinite (if p on axis)
 - Subproblem 2 - Rotate about 2 axis
 - $e^{\hat{e}_1 \theta_1} e^{\hat{e}_2 \theta_2} p = q$
 - 0, 1, 2 soln
 - Subproblem 3 - Rotate about 3 axis
 - $\|q - e^{\hat{e}_1 \theta_1} p\| = \delta$
 - 0, 1, 2 soln

- Tip
 - put point on axis to make stuff
 - put multiply by p to do so
 - also subtract point from both sides and take norm
 - careful to not overcomplicate if want them
- Extra
 - $e^A = \sum_{n=0}^{\infty} \frac{A^n}{n!} = I + A + \frac{1}{2!} A^2 + \dots$
 - $(e^A)^T = e^{A^T}$
 - $e^{g A g^{-1}} = g e^A g^{-1}$
 - e^A also eigenvalue of e^A
 - $(e^A)^{-1} = e^{-A}$
 - $\det(e^A) = e^{\text{tr} A}$

- ROS
 - made - executable that runs
 - topics - can publish message to/read from
 - services - request made to do stuff

- Computer Vision

- Pinhole Camera Model

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} \rightarrow \begin{bmatrix} u \\ v \end{bmatrix} = \frac{f}{z} \begin{bmatrix} X \\ Y \end{bmatrix}$$

$$\lambda \begin{bmatrix} x_{in} \\ y_{in} \\ z_{in} \end{bmatrix} = \begin{bmatrix} f f_x & f f_y & f \\ 0 & f f_y & f \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \end{bmatrix} = \begin{bmatrix} R & T \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} X_c \\ Y_c \\ Z_c \end{bmatrix}$$

scale factor λ pixel $\begin{bmatrix} u \\ v \end{bmatrix}$ intrinsic matrix $\begin{bmatrix} f f_x & f f_y & f \\ 0 & f f_y & f \\ 0 & 0 & 1 \end{bmatrix}$ camera location $\begin{bmatrix} R & T \\ 0 & 0 & 1 \end{bmatrix}$ PD $\begin{bmatrix} X_c \\ Y_c \\ Z_c \end{bmatrix}$

- aka $\lambda X = KX$ - in camera frame (X_c, Y_c, Z_c)
- $Z_c(x_c, y_c)$ always positive, never 0
- typically, all quantities for $\lambda X = X$ (not by K^{-1})
- Correspondence - Z-camera
- lots of assumptions about materials
- Epipolar constraint - apply to points & transform
- assume in camera is world from $X_c = R X_w + T$
- $X_c^T R X_w = 0$
- $T^T R$ - essential matrix
- has SVD $E = U E V^T$ w/ $E = \text{diag}(e, e, 0)$

- Computing essential matrix E
- 8 point linear algorithm
- work out $X_c^T E X_w = 0 \rightarrow A e = 0$
- need rank 8 matrix
- if A is rank 8 (Hough), $A^T A$ null λ
- E also null in essential space
- A is 8×8 $F_2 \in \mathbb{R}^2(x_1, x_2, x_3)^T$
- get $E = U \text{diag}(e, e, 0) V^T$
- minimize $\|E - F\|_F^2$ relative
- compute path E up to scale factor
- normalize T to unit vector
- $R = U R_2^T (E \frac{1}{e}) V^T$
- $T = U R_2^T U R_3 (T \frac{1}{e}) \in U^T$
- sanity check: duplicate positive e
- ph center in essential

- Rigid Body Velocities
- Spatial and body frames $A \in B$
- Spatial Velocity
- $\text{vel}^B q_c(t) = \dot{q}_c(t) q_c = \dot{q}_c(t) g_{q_c}^{-1}(t) q_c = \hat{V}_{q_c}^B q_c$
- $\hat{V}_{q_c}^B = \dot{q}_c q_c^{-1} = \begin{bmatrix} R_{q_c}^T \dot{R}_{q_c} & R_{q_c}^T \dot{P}_{q_c} \\ 0 & \dot{P}_{q_c} \end{bmatrix}$
- Body Velocity - put in body frame relative A vs B
- $\text{vel}^A(t) = g_{q_c}^{-1}(t) \dot{q}_c(t) q_c = \hat{V}_{q_c}^A q_c$
- $\hat{V}_{q_c}^A = g_{q_c}^{-1}(t) \hat{V}_{q_c}^B q_c$
- $\hat{V}_{q_c}^A = g_{q_c}^{-1} \dot{q}_c q_c^{-1} = \begin{bmatrix} R_{q_c}^T \dot{R}_{q_c} & R_{q_c}^T \dot{P}_{q_c} \\ 0 & \dot{P}_{q_c} \end{bmatrix}$
- $\hat{V}_{q_c}^A = g_{q_c}^{-1} \hat{V}_{q_c}^B g_{q_c}$
- $\hat{V}_{q_c}^A = A g_{q_c} \hat{V}_{q_c}^B$
- $A g_{q_c}^{-1} = \begin{bmatrix} R & \dot{P} \\ 0 & R^T \end{bmatrix}$

- $\text{Vel}^S = \text{Vel}^B + A \dot{g}_{q_c} \text{Vel}^B$ composition
- $\text{Vel}^S = A \dot{g}_{q_c}^{-1} \text{Vel}^B + \text{Vel}^B$
- can integrate w/ rectangles $[\Delta t]$ original + linear component
- Manipulator Jacobians
- Spatial Jacobian
- $\text{Vel}^S = J_{sp}^S(\theta) \dot{\theta}$
- $J_{sp}^S(\theta) = \begin{bmatrix} \frac{\partial g_{q_c}}{\partial \theta_1} & \dots & \frac{\partial g_{q_c}}{\partial \theta_n} \end{bmatrix}^T$
- $J_{sp}^S(\theta) = \begin{bmatrix} E_1 & E_2 & \dots & E_n \end{bmatrix}$
- $E_i = A d_{q_c} e_i \dots e_i \dots e_i \dots e_i$
- e_i usually transforms from reference frame

- Body Jacobian
- $\text{Vel}^B = J_{sp}^B(\theta) \dot{\theta}$
- $J_{sp}^B(\theta) = \begin{bmatrix} E_1 & \dots & E_n \end{bmatrix}^T$
- $E_i = A d_{q_c}^{-1} e_i \dots e_i \dots e_i \dots e_i$

- Singularities
- when Jacobian drops rank (usually when not full rank)
- not invertible, can't extract information in all directions, not force
- also singular -> need large velocities to get desired
- ure determinant $\det(A) \neq 0$ if invertible, $\text{rank}(A^T A) = \text{rank}(A) \leq \min(m, n)$

- Lagrangian Dynamics

- Pick parametrization q (usually θ)
- $T =$ kinetic energy
- $\frac{1}{2} m \dot{x}^2 + \frac{1}{2} I \dot{\theta}^2$ on helpful
- $V =$ potential energy
- mph, V like on helpful
- $L = T - V$ (Lagrangian)
- $\gamma = \frac{\partial L}{\partial \dot{q}} - \frac{\partial L}{\partial q}$
- fixed \dot{q} at $q =$ diff variable
- γ as joint forces/torques
- $\tau = M(\theta) \ddot{\theta} + C(\theta, \dot{\theta}) \dot{\theta} + G(\theta)$
- manipulator controls joint torque

- Control
- desired trajectory $\theta_d(t)$
- output $T = M \ddot{\theta} + C \dot{\theta} + G$
- let nothing perfect
- $T = M \ddot{\theta} + C \dot{\theta} + G$ (error)
- chattering, backstepping (PD controller)
- $\tau = M(\ddot{\theta}_d - K_v \dot{\theta} - K_p \theta) + C \dot{\theta} + G$
- $e = \theta - \theta_d$
- $\ddot{e} + K_v \dot{e} + K_p e = 0$ write feedback
- feedback + feedback K_v, K_p
- exponential tracking

- path planning
- w/ obstacles -> navigate configuration space
- cell decomposition - obstacles + grid nodes
- refine to avoid obstacles
- give via points
- interpolate to smooth out
- or approximate (spline)
- increase interpolation under other number
- not more complex via (like v, a, \dots)
- 1 - $\theta, \dot{\theta}, \ddot{\theta}$
- 2 - $\theta, \dot{\theta}, v, a, \ddot{\theta}$
- 3 - $\theta, \dot{\theta}, v, a, \ddot{\theta}$
- 5 - $\theta, \dot{\theta}, v, a, \ddot{\theta}, \dots$
- better to blend methods to get better (LPPB)

- minimum time trajectories (bang bang)
- A^* path search
- $C(x) = g(x) + h(x)$
- heuristic heuristic to goal
- but stops search points
- add extra to obstacles? but obstacles

- Probabilistic Road Map (PRM)
- random points, remove collisions
- connect all edges, remove collisions
- use A^*
- Rapidly Exploring Random Tree (RRT)
- branch & bound unexplored (Voroni)
- suboptimal at
- branch by step increasing suboptimal
- RRT* - rewired nodes, asymptotically optimal
- other RRT variants

- shooting - like a cannon shot see if hit
- \dot{x} use via method
- Direct Transcription ZOH, q
- Direct Collocation - poly on trajectory

- Labs
- bag - completed April
- point cloud - robot points
- image registration
- thresholding
- edge detection
- clustering
- can synchronize two w/ approximate time
- Richman lab
- decouple - BRPSS
- neural network
- learning - stable for xpt
- occupancy grid - low RAM work
- tracking probe
- autonomous - sensor enabling

Sampling based planners

optimization planners (BnB)